GENERAL NOTES:	4.0 MATERIALS	TOOLED -50
1.0 STANDARDS AND REFERENCES	4.1 CONCRETE	EDGE
THE FOLLOWING SHALL GOVERN THE DESIGN, FABRICATION AND CONSTRUCTION OF THE PROJECT.	4.1.1 CONCRETE COVER OVER REINFORCING BARS SHALL BE AS FOLLOWS: A. FOOTINGS, FOOTING-TIE BEAMS (CAST AGAINST EARTH) 75mm	
1.1 NATIONAL STRUCTURAL CODE OF THE PHILIPPINES (N.S.C.P.). VOL. 1, 6TH EDITION, 2010.	B. BEAMS AND COLUMNS (TO STIRCUPS AND TIES) 40mm C. WALLS, SIDE OF FOOTING-TIE BEAMS (CAST AGAINST FORMS) 40mm	
2.0 DESIGN CRITERIA	D. SUSPENDED SLAB 20mm	CONSTRUCT
2.1 LOADINGS A. DEAD LOAD	4.1.2 BEFORE CONCRETE IS POURED, CHECK WITH ALL TRADES TO ENSURE PROPER PLACEMENT OF ALL OPENINGS, SLEEVES, CURBS, CONDUITS, ETC. RELATING TO	SAWED JOINT W/ SEALANT
CONCRETE –23.56kN/m ³ STEEL –76.93kN/m ³	THE WORK. 4.2 REINFORCING BARS	
150mm THK. CHB WALL –2.73 kPa 100mm THK. CHB WALL –2.11 kPa	4.2.1 ALL REINFORCING BARS SHALL BE CLEAN OF RUST, GREASE OR OTHER MATERIALS	
B. LIVE ROAD ROOF -1.00 kPa	THAT WILL IMPAIR BOND.	WEAKENED P
SLAB ON GROUND -4.80 kPa	4.2.2 ALL REINFORCING BARS SHALL BE ACCURATELY AND SECURELY PLACED BEFORE POURING CONCRETE OR APPLYING MORTAR OR GROUT.	NOTE: CONTROL JOINT CAN BE OR WEAKENED PLANE JO
	4.2.3 LAPPED SPLICES SHALL BE STAGGERED WHERE POSSIBLE.	
C. WIND LOAD (NSCP 2010)	4.2.4 UNLESS OTHERWISE INDICATED, SPLICING OF REINFORCEMENT SHALL BE IN ACCORDANCE WITH ACI-318M, EXCEPT THAT THE MINIMUM LAP SPLICE SHALL BE	
BASIC WIND VELOCITY, V = 250 KPH P = qh [(GCpf)-(GCpi)] (DESIGN WIND PRESSURE) WHERE: $qh = VELOCITY PRESSURE, kPq)$	40 BAR DIAMETER BUT NOT LESS THAN 600mm.	
GCpf = EXTERNAL PRESSURE COEFFICIENT GCpf = INTERNAL PRESSURE COEFFICIENT	4.2.5 UNLESS SHOWN OTHERWISE ON PLANS, SPLICES SHALL BE AS FOLLOWS: A. INTERMEDIATE BEAMS: TOP BARS SHALL BE SPLICED AT MID-SPAN, AND BOTTOM	2 CONTROL JOINTS
D. SEISMIC LOAD (NSCP 2010)	BARS AT THE SUPPORT. B. BEAMS FRAMING TO COLUMNS: TOP BARS SHALL BE SPLICED AT MID-SPAN AND	+
$V = \frac{CM^2}{RT} W$ (DESIGN BASE SHEAR)	BOTTOM BARS SHALL NOT BE SPLICED W/IN THE COLUMN OR W/IN A DISTANCE OF TWICE THE MEMBER DEPTH FROM THE FACE OF THE COLUMN. THE SPLICED	
$Vmax = \frac{2.50 \text{ Cal}}{R} \text{ W} Vmin = 0.11 \text{ CalW}$	LENGTH SHALL NOT BE LESS THAN 1.4 TIMES THE DEVELOPMENT LENGTH (Ld) IN 4.2.8 BELOW BUT NOT LESS THAN THAN 600mm THE CONVENTION OF A DEVELOPMENT AND CONVENTION OF A DEVELOPMENT	
$Vmin = \frac{0.80 \text{ ZNvl}}{\text{R}} \text{ W (ZONE 4)}$	C. COLUMNS: LAP SPLICES SHALL BE MADE WITHIN THE CENTER HALF OF HEIGHT AND THE SPLICE SHALL NOT BE LESS THAN 30 BAR DIAMETER. WELDING OR THE USE OF APPROVED MECHANICAL DEVICES MAY BE PERMITTED PROVIDED	
WHERE: W = TOTAL DEAD LOAD T = NATURAL PERIOD = C, $(h_n)^{2/3}$;	NOT MORE THAN ALTERNATE BARS ARE WELDED OR SPLICED AT ANY LEVEL AND THE MINIMUM VERTICAL DISTANCE BETWEEN TWO ADJACENT BAR SPLICES SHALL	
WHERE: C = NUMERICAL COËFFICIENT h = BUILDING HEIGHT	BE 600mm. D. CHB WALLS: VERTICAL BARS SHALL BE SPLICED AT THE TOP OF WALL FOOTINGS	
I = IMPORTANCE FACTOR = 1.50 $R = NUMERICAL FACTOR = 8.50$	OR FOOTING-TIE BEAMS AND AT THE BOTTOM OF REINFORCED CONCRETE LINTEL BEAMS OR BEAMS.	90° HOOK 180° H
SEISMIC COEFFICIENT CV = 0.44 NV Ca = 0.64 N NEAR SOURCE FACTOR (10km) NV = 1.2	4.2.6 UNLESS OTHERWISE INDICATED: ALL BEAMS TERMINATING AT A COLUMN SHALL HAVE TOP AND BOTTOM BARS EXTENDING TO THE FAR FACE OF THE COLUMN, TERMINATING	BAR SIZE
$N_0 = 1.0$ Z = SEISMIC ZONE = 0.40 (ZONE 4)	IN A STANDARD 90 HOOK LENGTH OF ANCHORAGE SHALL NOT BE LESS THAN 600mm. 4.2.7 SHOP DRAWING FOR REINFORCEMENT SHALL BE SUBMITTED FOR APPROVAL OF THE	
S = SOIL TYPE = D	4.2.7 SHOP DRAWING FOR REINFORCEMENT SHALL BE SUBMITTED FOR APPROVAL OF THE ENGINEER PRIOR TO FABRICATION & INSTALLATION.	10mm Ø THRU 25mm Ø 28mm Ø THRU 36mm Ø
2.2 DESIGN STRESSES A. CONCRETE	4.2.8 DEVELOPMENT LENGTH (Ld) OF REINFORCING BARS SHALL BE AS FOLLOWS: SIZE OF REBARS DEVELOPMENT LENGTH	NOTE: 1. ALL BENDS SHOWN IN I
COMPRESSIVE STRENGTH @ 28 DAYS fc' = 20.7 MPa (3,000 psi) B. REINFORCING BARS a. FOR BARS 16mm ø AND GREATER fy = 275 MPa (40,000 psi)	10 mm 170 mm 12 mm 220 mm	STANDARD HOOK OTHER
b. FOR BARS LESS THAN 16mm ø fy = 230 MPa (33,000 psi) C. STRUCTURAL STEEL, ASTM-A36	16 mm 270 mm 20 mm 380 mm	2. 180' HOOKS MAY BE S
FOR TRUSSES, BRACINGS, & STRUTS $fy = 248 \text{ MPg} (36,000 \text{ psi})$ D. PURLINS	25 mm 600 mm 4.3 STRUCTURAL STEEL	
COLD FORMED LIGHT GAGE SHAPES $fy = 248 \text{ MPo} (36,000 \text{ psi})$ E. MASONRY UNIT (CHB) NON-LOAD BERRING CHB WALLS $fm' = 3.45 \text{ MPo} (500 \text{ psi})$	4.3.1 ALL STRUCTURAL STEEL SHALL CONFORM TO ASTM A36 AND SHALL HAVE A MINIMUM	WIF
F. WELDS-USED E-60x ELECTRODE G. STRUCTURAL BOLTS, ASTM-A307 a. Ft = 96.60 MPa (14,000 psi) b. Fv = 69 MPa (10,000 psi)	YIELD STRESS, Fy = 248 MPa (36,000 psi) 4.3.2 ALL STRUCTURAL STEEL SHALL BE FABRICATED AND ERECTED IN ACCORDANCE WITH THE AISC SPECIFICATIONS AND CODE OF STANDARD PRACTICE AS AMMENDED TO DATE.	OFFSET
3.0 FOUNDATION	4.3.3 ALL BOLTS SHALL CONFORM TO ASTM A-307 UNLESS OTHERWISE INDICATED. 4.3.4 SHOP AND FIELD WELDING SHALL BE IN ACCORDANCE WITH AWS D1.1 AND PERFORMED	3 TYP. REINFOR
3.1 ASSUMED SOIL BEARING CAPACITY SHALL BE 96KPo (2,000 PSF)	BY QUALIFIED WELDERS. 4.3.5 UNLESS OTHERWISE INDICATED, WELDING ELECTRODES SHALL BE E60.	
3.1.1 IN CASE THE ACTUAL LOCATION OF THE STRUCTURE IS LESS THAN THE ASSUMED DISTANCE FROM THE SEISMIC SOURCE OF 40km; NOTIFY THE DIRECTOR, BUREAU DISTANCE FROM THE SEISMIC SOURCE OF AUGMENTATION DEFECTION, BUREAU	4.3.6 NO STEEL SHALL BE FABRICATED OR ERECTED UNTIL SHOP DRAWINGS HAVE BEEN APPROVED BY THE STRUCTURAL ENGINEER. 4.3.7 WELDS/(CONFORM WITH AMERICAN WELDING STANDARDS) USING E 60xx ELECTODES.	1
OF DESIGN FOR PROPER REVISION OF THE DESIGN. REFER TO THE SEISMIC SOURCE MAP PROVIDED IN THE NATIONAL STRUCTURAL CODE OF THE PHILIPPINES OR PHIVOLCS SEISMIC SOURCE MAP.	4.3.7 WELDS/CURFORM WITH AMERICAN WELDING STANDARDS) USING E 60xx ELECTODES. $f_y = 93.77$ MPa. 4.3.8 ANCHOR BOLTS (CONFORM WITH ASTM A-307) ft = 96.60 MPa. fv = 69 MPa.	
OR PHIVOLOS SEISMIC SOURCE MAP. 3.1.2 SOIL TEST SHALL BE CONDUCTED PRIOR TO START OF CONSTRUCTION. 3.1.3 IN CASE THE ACTUAL SOIL BEARING CAPACITY IS FOUND LESS THAN THE ASSUMED.	4.3.6 ANCHOR BULIS (CONFORM WITH ASIM $A = 307$) It = 96.60 MPd. IV = 69 MPd.	0INT - 50 30 50 3 EXTRA STIRRUP
96 KPG; NOTIFY THE DIRECTOR, BUREAU OF DESIGN FOR PROPER REVISION OF FOUNDATION.	4.4 CONCRETE HOLLOW BLOCKS (CHB):	
3.1.4 NO FOOTING SHALL REST ON FILL. 3.1.5 BOTTOM OF FOOTING SHALL BE AT LEAST 1.00m. BELOW NATURAL GRADE LINE. 3.1.6 SOUL BEADING CHARGITY SHALL BE INCREASED BY 33% WHEN IN COMPINITION WITH	4.4.1 UNLESS OTHERWISE INDICATED, CHB USED IN THIS WORK SHALL HAVE A MINIMUM ULTIMATE COMPRESSIVE STRENGTH f'm = 3.45 MPa (500 psi)	
3.1.6 SOIL BEARING CAPACITY SHALL BE INCREASED BY 33% WHEN IN COMBINATION WITH SEISMIC OR WIND LOAD.	4.4.2 ALL CHB CELLS SHALL BE FILLED SOLIDLY WITH GROUT.	
3.2 ALL COLUMN FOOTINGS & TIE BEAMS SHALL REST ON 100mm THK. WELL COMPACTED GRAVEL BASE COURSE.	5.0 CONSTRUCTION JOINT 5.1 CONSTRUCTION JOINT NOT INDICATED ON THE PLANS SHALL BE MADE SO AS TO LEAST	
3.3 BACK FILL SHALL BE PLACED IN LAYER AND EACH LAYER SHALL BE 200mm THK. AND SHALL BE COMPACTED TO 95% MAXIMUM DRY DENSITY.	5.1 CONSTRUCTION JUINT NOT INDICATED ON THE PLANS SHALL BE MADE SO AS TO LEAST IMPAIR THE STRENGTH OF THE STRUCTURE AND SHALL BE SUBJECT TO THE APPROVAL OF THE ENGINEER EXCEPT SLAB ON GRADE.	BEAM REINFORCEMENT (DO NOT INTERRI
3.4 WHERE LOOSE/SOFT MATERIAL IS ENCOUNTERED AT DEPTH OF EMBEDMENT INDICATED, EXCAVATE TO FIRM LAYER AND REPLACE LOOSE/MATERIALS UNDERNEATH THE FOOTING	5.2 UNLESS SHOWN OTHERWISE, SLAB ON GRADE SHALL HAVE CONTROL JOINTS SPACED AT 6000mm MAXIMUM CENTER TO CENTER.	
WITHIN THE FOOTING AREA PLUS 1/2 DEPTH OF SOFT MATERIAL ON ALL SIDES WITH SELECT GRANULAR BACKFILL. COMPACT SELECT GRANULAR BACKFILL TO 95% OF	5.3 BEAMS CONSTRUCTION JOINT SHALL BE LOCATED W/ IN THE MIDDLE THIRD OF THE SPAN. IT SHALL BE PROVIDED WITH 3 EXTRA STIRRUPS @ 75mm 0.C. ON EACH SIDE OF THE	BEAM CONSTRUCTION JOI
MAXIMUM DRY DENSITY.	II SHALL BE PROVIDED WITH 3 EXTRA STIRROPS @ 75mm U.C. UN EACH SIDE OF THE	OT TO SC
	1 GENERAL NOTES & STANDARD DETAILS	
	S NOT TO SCALE	
SHEET CONTENT: PREPARED BY:	PROJECT TITLE AND LOCATION:	APPROVED AS PER PLAN:
SOUTHER LEYTE STATE CONSTRUCTION	PROPOSED REPAIR AND IMPROVEMENT OF	
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